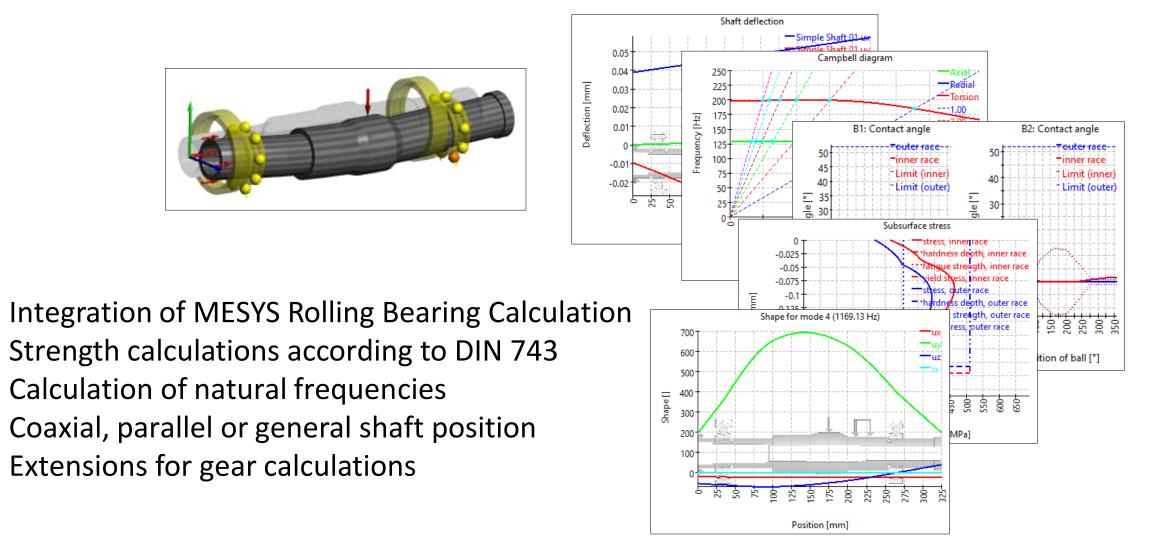
MESYS Shaft Calculation





Shaft calculation



- The shaft calculation allows the calculation of bearing forces and tilting angles for a system of coaxial shafts.
- Bearings can be connected with a housing or with a second shaft.
- All inputs of the rolling bearing calculation are available in the shaft calculation.
- The calculation of natural frequencies is possible considering nonlinear bearing stiffness.
- The calculation can be run using load spectra.



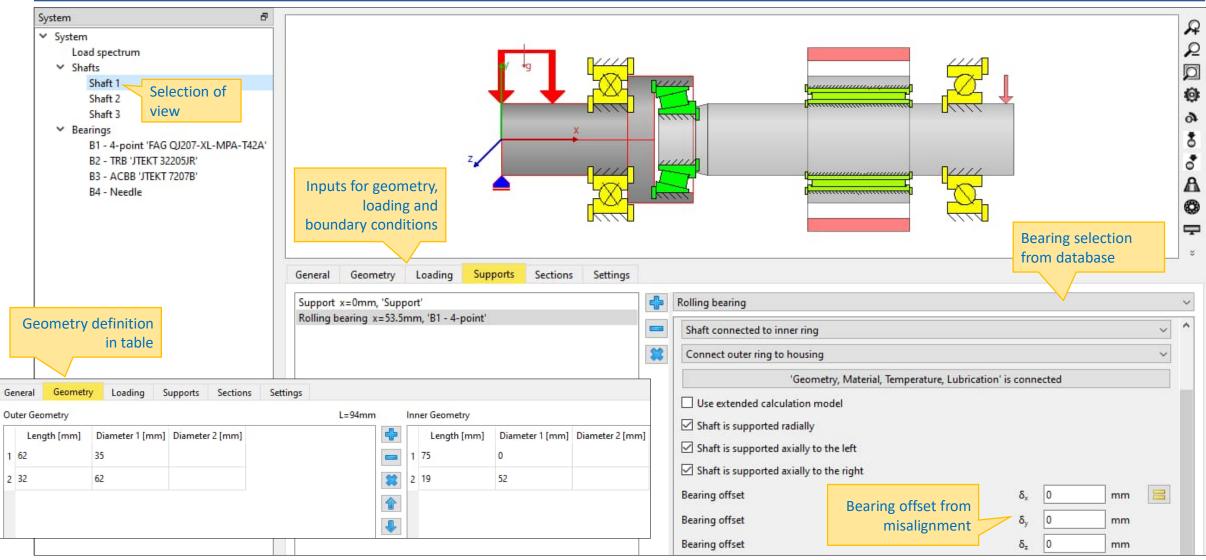
- The shaft deflection is calculated using finite element beam elements (optionally geometrically nonlinear, considering shear deformations).
- Rolling bearings are coupled to single nodes at inner and outer race.
- Thermal elongations and axial shaft deformation are considered.
- In the calculation of natural frequencies, the inertia of the shaft is considered and optionally the gyroscopic effect.



	MOSUS Engineering Consulting Software	Shaft Calculation			
Default values for lubrication	Project name Weight is considered optionally Calculation description optionally Settings Lubrication ✓ Consider weight Angle for weight β _w ✓ Calculate natural frequencies	Image: Material and temperature for housing Image: Mousing material Image: Steel Image: Mousing temperature I	r		
	 ☐ Consider gyroscopic effect Maximum frequency Mumber of frequencies ☐ Consider gears as stiffness ☐ Consider gears as point load ☐ Consider housing stiffness 	Bearing position Definition for each bearing Shear deformations According Hutchinson of Consider nonlinear shaft model Consider load spectrum According Hutchinson			

Shaft calculation user interface





Shaft calculation Rolling bearings



ystem 🗗	General Bea	ring geometry Bearing configuration	n Material	and Lubri	cation	Loading	Track roller
System	General	beaming configuration	in Materia		cation	Loading	INSEK TONET
✓ Shafts	Four point ball	bearing (radial)				~ 🕂	Select bearing from database 🗸 🗸
Shaft 1 Shaft 2 Bearing	Inner diameter		d	35	mn	n 🔶 🗆	Dynamic load rating Cr 45 kN
Shaft 3 Selection	Outor Franks			73	_		Static load rating COr 35.5 kN
✓ Bearings	Outer diameter		D	72	mn	n 🕂 🗆	
B1 - 4-point 'FÁG QJ207-XL-MPA-T42A'	Manufacturer	name	di [mm]	De [mm]	B [mn	n] alph; ^	Fatigue load limit Cur 2.47 kN
B2 - TRB 'JTEKT 32205JR' B3 - ACBB 'JTEKT 7207B'	FAG	QJ207-XL-MPA-T42A	35	72	17	35	Bearing clearance User input as operating clearance \vee
B4 - Needle	FAG	QJ207-XL-MPA-S1-T42A	35	72	17	35	Axial clearance Pa 0 µm 🚍
	FAG	QJ207-XL-MPA-C3-M32G	35	72	17	35	Rolling bearing
	FAG	QJ207-XL-MPA-C3	35	72	17	35	Name B1 - 4-point
	FAG	QJ207-XL-MPA-C2	35	72	17	35	Position x 53.5 mm
	FAG	QJ207-XL-MPA	35	72	17	35	Type Four point ball bearing (radial) (FAG QJ207-XL-MPA-T42A)
	FAG	QJ206-XL-N2-MPA-T42B	30	62	16	35	Shaft connected to inner ring
	FAG	QJ206-XL-N2-MPA-T42A	30	62	16	35	Connect outer ring to housing
	FAG	QJ206-XL-N2-MPA-P6-T42B	30	62	16	35	'Geometry, Material, Temperature, Lubrication' is connected
	FAG	QJ206-XL-MPA-T42A	30	62	16	35 🗸	Use extended calculation model
	<						

If the bearing calculation is activated, then File>Load or File>Save are only referencing the bearing calculation data. In this way existing bearing calculation files can be imported.

Using Ctrl-F5 runs the whole system calculation.

Shaft is supported axially to the right

Bearing offset

Bearing offset

Bearing offset

mm

mm

mm

δ, 0

δ_z 0

δ

0

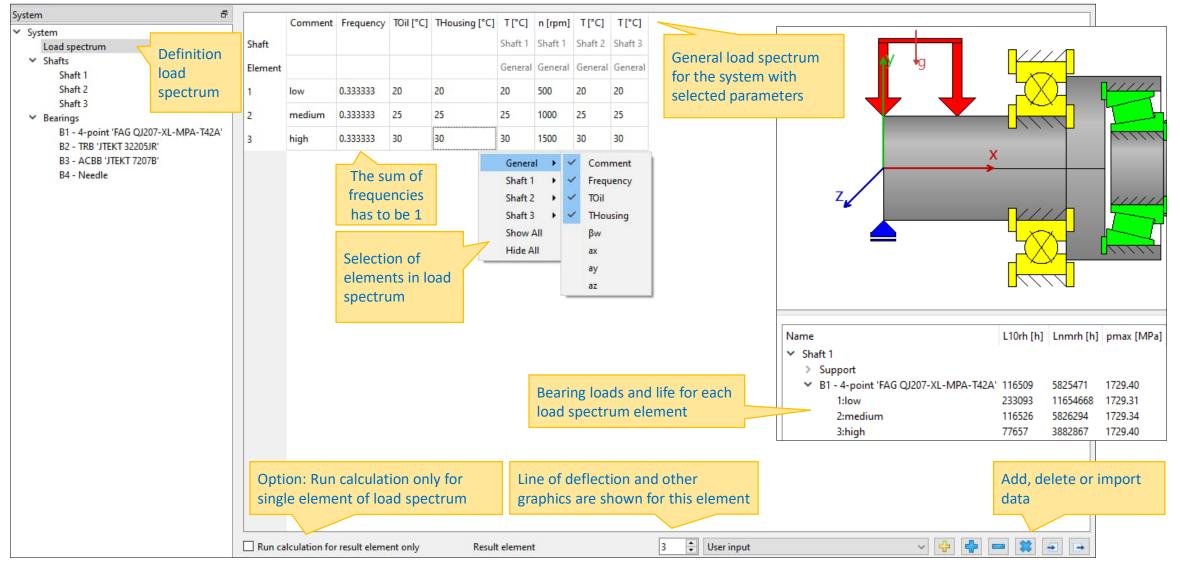
Shaft calculation Load elements



Cylindrical gear			•]	Cylindrical gear				-	
Name	x	20	mm		Force Coupling Cylindrical gear Excentric force					Available load elements
Width	Ь	40	mm	Direction of torque	Mass				-	
Torque Direction of torque	T Own I	2000 input	Nm	with sign, driving or driven	Name					
Angle to contact Number of teeth	ζ z	0	° 🔨	Position gear contact.	Position Width	x	30	mm		In case of a width > 0, the mass is distributed on
Normal module Normal pressure angle	mn	3	mm	0° - on y-axis 90°-on z-axis	Mass	b m	20 5	mm kg		a line
Helix angle	α _n βn	20 0	•	Optional data for	Mass moment of inertia Mass moment of inertia	Jxx Jyy		kg m² kg m		Mass moment of inertia are optional
Helix direction Number of teeth of mating	Spurg gear z2	gear 0	•	mating gear. If available the	Mass moment of inertia	Jzz		kg m²		
Center distance	a	0	mm	operating pitch diameter is used for calculation of forces	A line mass an					ertia. This is considered in the nertia has to be used as input.

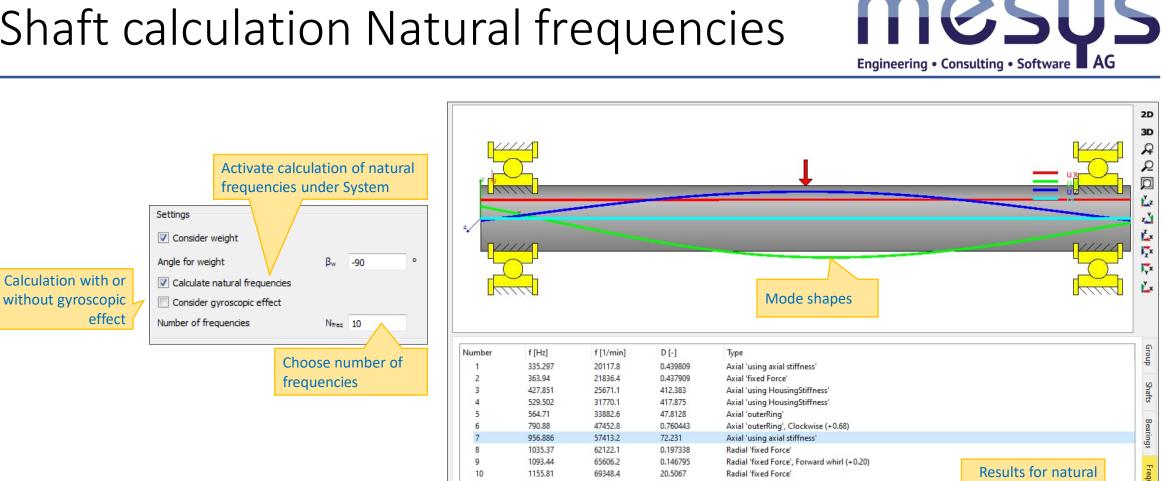
Shaft calculation Load spectra





MESYS AG - Technoparkstrasse 1 - 8005 Zürich

Shaft calculation Natural frequencies

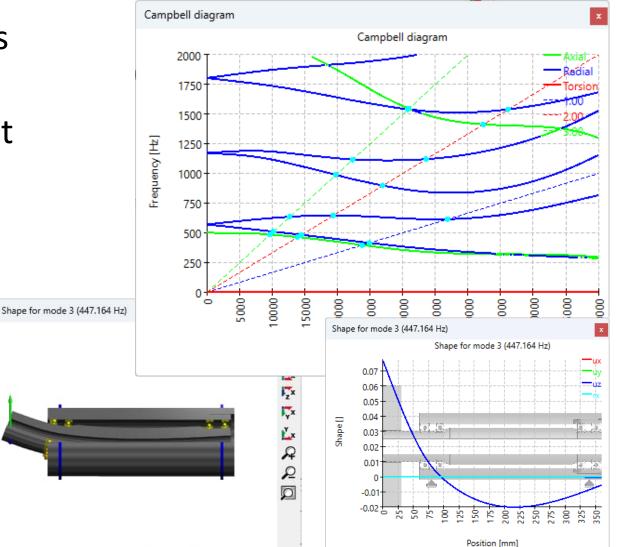


The calculation of natural frequencies is done at equilibrium under defined load conditions, the bearing stiffness in this working point is used.

frequencies

Shaft calculation Natural frequencies

- Calculation of natural frequencies for given speeds
- Consideration of gyroscopic effect and speed dependent bearing stiffness
- Campbell diagram
- Critical speeds
- Mode shapes as 2D-diagram and 3D-Animation

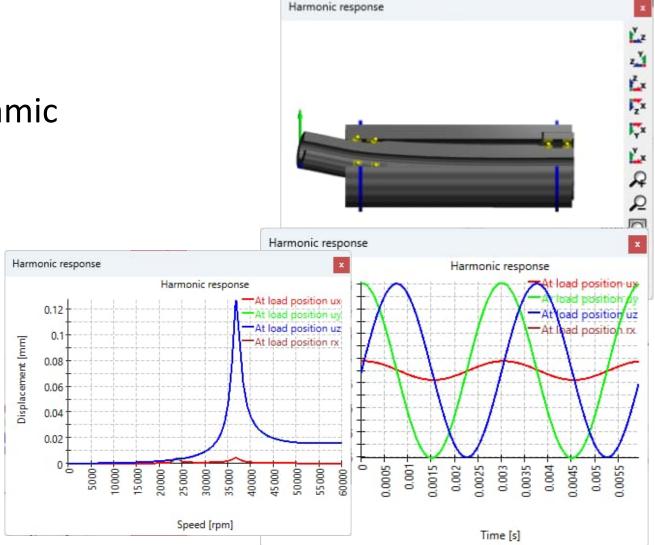




11

Shaft calculation Harmonic response

- Harmonic response to dynamic forces
- Excitation as imbalance or dynamic force
- Base excitations for supports
- Gear mesh excitations
- Results as amplitudes, velocities and forces
- Diagrams over rotations speed or over time
- 3D-Animation





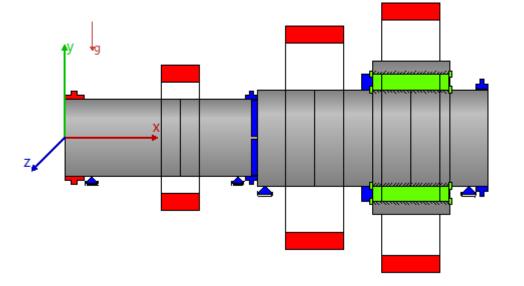




- For each shaft, it is possible to define either a unique temperature, or a temperature gradient by adding a temperature difference 'ΔT'(±) for those elements created at the outer geometry. The temperature of the housing can be defined as well.
- From the thermal expansions arise axial displacements of the shafts and also, depending on the bearing, axial forces.
- The temperatures are also transferred to the bearing calculation thus having influence on the bearing clearance.

Shift gearboxes

- Idler-wheels in shift gearboxes can be set either as spur gear on the shaft or as idle wheel shaft with a bearing and a general constrain.
- Through configurations, it is possible to deactivate single components for certain gear connections.
- Important: For the created couplings, the rotational degree of freedom must be fixed. Then, at configurations this constraint can be voided.



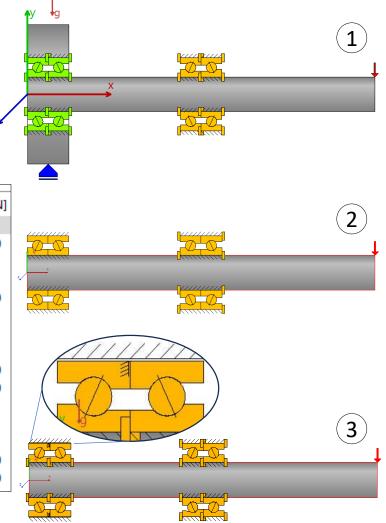
	Name	Direktgang	Syncronring	G1a-G1b
1	G1			1
2	G2		1	
3	G3	V		



Spindle bearings Sets of bearings

- Variant 1: Define all the bearings on the shaft, use a hollow shaft to perform the role of non-locating bearing.
- Variant 2: Place two bearings on the shaft and use bearing configurations in the bearing calculation. Shorter lives are to be expected here, since it is calculated as double-row bearing.
- Variant 3: The 'extended calculation' model is used. A hollow shaft is not required in this case, as the positional relationships of both rings to all adjacent components can be defined.

		-						
Na	me	L10rh [h]	Lnmrh [h]	pmax [MPa]	S0eff	Fx [N]	Fy [N]	Fz [N]
~	OuterRing							
	Support					0.00	708.81	-0.00
~	Shaft 1							
	B1.1 'Generic 7004D'	280623	5430452	1454.80	24.06	212.58	302.04	0.00
	B1.2 'Generic 7004D'	93423	827954	1721.09	14.57	-212.58	413.50	-0.00
	B1.3 'Generic 7004D'	13246	40616	1976.06	9.41	908.02	527.99	0.00
	B1.4 'Generic 7004D'	579	567	3020.28	2.69	-1208.02	-2248.37	0.00
~	Shaft 2							
	B2.1 'Generic 7004D'	83741	949646	1685.90	15.49	-0.00	700.80	-0.00
	B2.2 'Generic 7004D'	550	545	3027.38	2.67	-300.00	-1705.64	-0.00
~	Shaft 3							
	B3.1 'Generic 7004D'	280391	5422427	1455.19	24.04	212.28	302.28	0.00
	B3.2 'Generic 7004D'	93662	831430	1720.66	14.58	-212.28	413.13	0.00
	B3.3 'Generic 7004D'	13243	40603	1976.13	9.41	908.04	528.12	-0.00
	B3.4 'Generic 7004D'	579	567	3020.28	2.69	-1208.04	-2248.38	-0.00



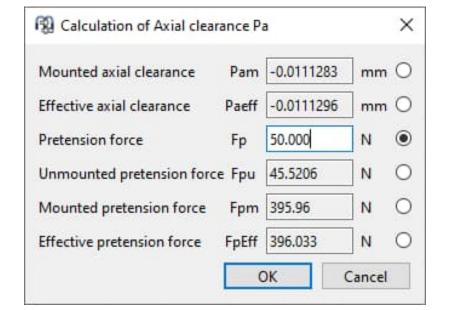


Bearing preload

- A pretension can be entered by using a negative value for the axial clearance Pa, which is shown for angular contact bearings, tapered roller bearings, four-point bearings, cylindrical roller bearings and all axial bearings.
- If with angular contact bearings or tapered roller bearings 'User input' is chosen for 'Bearing clearance', the axial clearance can also be calculated for a given pretension force.

Dependent on the bearing type, several options for the pretension force are available:

- The calculation with "Fp" is using nominal dimensions for the bearings.
- The calculation using "Fpu" is using nominal dimensions together with a radial elastic expansion without limit.
- The mounted pretension force "Fpm" is calculated using the dimensions after fitting but no temperature or speed.
- The effective pretension force "FpEff" is calculated using the dimensions after fitting and considering temperature and speed.



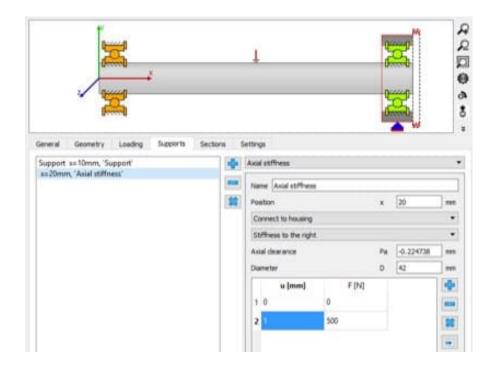


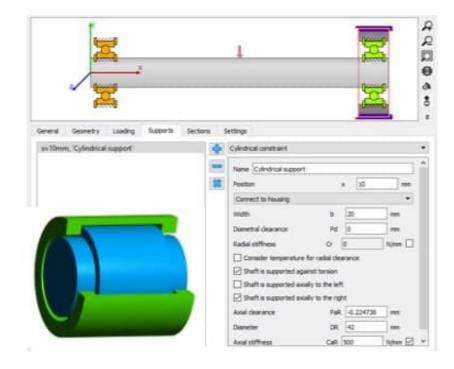
Bearing preload



A new axial stiffness allows the input of a nonlinear A cylindrical constraint allows to define a radial stiffness. The axial stiffness is distributed over a diameter, therefore a moment load can be taken in case of axial load.

clearance of a shaft in a tube. Additionally an axial contact can be defined distributed over a diameter.





- In the past, in order to take into account the housing stiffness in addition to the bearing stiffness, an "Outer-ring shaft" had to be added. Then, this shaft was connected to the rigid environment by means of a general constraint or a stiffness matrix.
- Additionally, it is possible to define directly a housing stiffness matrix. Both for global and local coordinate system, multiple symmetric stiffness matrices can be defined between the supports (only those which are connected to the housing) and the housing, thus acting as boundary condition at its connecting point. This enables the user to simulate different ways of stiffness interaction, also between the bearings or supports by means of the housing. Furthermore, is possible to apply a predefined force, moment, displacement or rotation for the connecting points in any of the three directions, as well as to consider rotation stiffness.
- A housing stiffness can be defined using an imported 3D-STEP housing or a Nastran-mesh.





- For documentation points on shafts a stiffness can be calculated.
- The resulting stiffness values cxx, cyy, czz, crx, cry, crz are the reciprocals of the main diagonals of the compliance matrix of the selected point.
- This corresponds to the determination of a stiffness by using a testing force and a displacement in the direction of the test force: Cyy = $\Delta Fy/\Delta uy$

General	Geometry	Loading	Supports	Sections	Settings				
Docume	ntation point	x=0mm, 'S	ection'			Documentation point Name Section Position Calculate stiffness	x	0	mm

Shaft strength according DIN 743 (2012)



- For strength calculation according DIN 743 the material and a few other parameters have to be selected.
- Cross sections can be defined on page «Sections».
- The number of load cycles is calculation from rotation speed and required life as default.

General					Strength				
Name Shaft Material	Steel			• •	Load factor (static) Load factor (fatigue)	KA_S KA_F	1200	2	0
Position		3	x 0	mm	Overload case	Constant str	-		•
Speed		n	0	rpm 🗌	Diameter at heat treatment	d _{at}	0	mm	0
Temperature		1	20	°C	Number of load cycles	N	1	10*	1
					Factor for surface work-hardening	KV	1		5
					Stress ratio, tension	Pulsating	*	0	
					Stress ratio, bending	Alternating	, *	-1	
					Stress ratio, torsion	Pulsating	÷	0	



- Technological size factor K1 for reduction of material strength
- Geometrical size influence for stress gradient in bending and torsion
- Notch factor
- Surface roughness and surface hardening
- Influence of mean stress
- Tension, bending and torsion are taken into account
- Calculation for load spectra or limited life

Shaft strength according DIN 743 (2012)

- Two options for calculation of permissible amplitude are available
- The option «constant stress ratio» is on the safe side
- As the equivalent mean stress is used, torsion will influence permissible bending stress

